

超混沌复系统的自适应广义组合复同步及参数辨识

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摘要: 该文针对含未知参数的异结构超混沌复系统, 基于自适应控制及 Lyapunov 稳定性理论, 提出一种新的自适应广义组合复同步方法 (GCCS)。首先给出广义组合复同步的定义, 将驱动-响应系统的同步问题转化为误差系统零解的稳定性问题; 然后从理论上设计了非线性反馈同步控制器及参数辨识更新律, 并引入误差反馈增益, 以控制同步的收敛速度; 最后以超混沌复 Lorenz 系统、超混沌复 Chen 系统、超混沌复 Lü 系统的广义组合复同步与参数估计为例, 从数值仿真角度验证了所提方法的正确性和有效性。

关键词: 超混沌复系统; 广义组合复同步; 参数辨识; 自适应控制

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Adaptive Generalized Combination Complex Synchronization and Parameter Identification of Hyperchaotic Complex Systems

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Abstract: Based on adaptive control and Lyapunov stability theory, a novel adaptive Generalized Combination Complex Synchronization (GCCS) scheme is proposed for nonidentical hyperchaotic complex systems with unknown parameters. Firstly, the definition of GCCS is presented, and synchronization of drive-response systems is transformed to the zero solution analysis of the error dynamical system. Secondly, a nonlinear feedback controller and parameter update laws are theoretically designed, wherein error feedback gains are introduced to control synchronization speed. Finally, GCCS among the hyperchaotic complex Lorenz system, complex Chen system, and complex Lü system is carried out to verify the correctness and effectiveness of the proposed scheme by numerical simulation.

Key words: Hyperchaotic complex systems; Generalized Combination Complex Synchronization (GCCS); Parameter identification; Adaptive control

1 引言

自1990年 Pecora 和 Carrol 提出混沌同步概念以来^[1], 混沌同步因其在保密通信、信号与信息处理、神经网络、生物工程等各领域具有广泛的应用潜能, 而受到持续关注并得到了广泛深入的研究, 从而成为自然科学、工程技术乃至社会科学等众多学科相互交叉的研究前沿和热点^[2-6]。与混沌实系统相比, 混沌复系统具有更加复杂的动力学行为, 将其运用

于保密通信, 既可以提高信息传输效率, 又可以提高抗攻击、抗破译等安全性能。因此, 近年来混沌复系统的同步研究备受瞩目, 混沌复系统、超混沌复系统的完全同步^[7]、反同步^[8]、延迟同步^[3,9]、相同步^[10]、投影同步^[11,12]、广义同步^[13]、组合同步^[14-16]等相继实现。

在上述同步类型中, 与其他单驱动单响应系统同步不同, 组合同步采用多个驱动系统驱动单个响应系统实现混沌同步, 其优点在于可以将传输信号进行分割后调制到不同的驱动系统, 或分时采用不同的驱动系统进行信号传输, 从而提高混沌保密通信的安全性和灵活性^[17]。文献[14]分别实现了3个同构、异构超混沌复系统的组合同步, 同步比例因子为实对角矩阵; 文献[15]实现了3个同构超混沌复系统的组合复同步, 同步比例因子为复对角矩阵; 文

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献[16]实现了不同阶非线性复系统、实系统间的组合复同步, 同步比例因子为复矩阵。

上述复系统组合同步、组合复同步中, 复系统的参数均为已知, 且同步比例因子均为不含时间和变量的系数矩阵, 而目前鲜见文献报道含未知参数复系统的广义同步、自适应组合同步。因此, 本文将针对一类含有未知参数的异结构超混沌复系统, 提出一种综合广义同步^[18]与组合同步的自适应广义组合复同步及参数估计方法, 基于自适应控制和 Lyapunov 稳定性理论设计非线性反馈控制器及参数辨识更新律, 并以超混沌复 Lorenz 系统、超混沌复 Chen 系统、超混沌复 Lü 系统的广义组合复同步及参数辨识为例, 验证所提方法的正确性和有效性。

2 广义组合复同步定义

考虑如下的非线性复系统分别作为驱动系统和响应系统:

$$\dot{\boldsymbol{x}} = \boldsymbol{F}(\boldsymbol{x})\boldsymbol{A} + \boldsymbol{f}(\boldsymbol{x}) \quad (1)$$

$$\dot{\boldsymbol{y}} = \boldsymbol{G}(\boldsymbol{y})\boldsymbol{B} + \boldsymbol{g}(\boldsymbol{y}) \quad (2)$$

$$\dot{\boldsymbol{z}} = \boldsymbol{H}(\boldsymbol{z})\boldsymbol{C} + \boldsymbol{h}(\boldsymbol{z}) + \boldsymbol{u}(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) \quad (3)$$

其中, $\boldsymbol{x} = (x_1, x_2, \dots, x_{m_1})^\top$, $\boldsymbol{y} = (y_1, y_2, \dots, y_{m_2})^\top$, $\boldsymbol{z} = (z_1, z_2, \dots, z_m)^\top$ 分别是驱动系统式(1), 驱动系统式(2)及响应系统式(3)的复状态向量, 则 $x_l = x_{l,r} + jx_{l,i}$ ($l=1-m_1$), $y_l = y_{l,r} + jy_{l,i}$ ($l=1-m_2$), $z_l = z_{l,r} + jz_{l,i}$ ($l=1-m$), $j = \sqrt{-1}$, 下标 r, i 在本文中分别表示复状态变量、向量、矩阵、函数的实部和虚部; $\boldsymbol{A} = (a_1, a_2, \dots, a_{m_1})^\top$, $\boldsymbol{B} = (b_1, b_2, \dots, b_{m_2})^\top$, $\boldsymbol{C} = (c_1, c_2, \dots, c_m)^\top$ 是未知参数实向量; 复矩阵 $\boldsymbol{F}(\boldsymbol{x}) \in \mathbf{C}^{m_1 \times m_1}$, $\boldsymbol{G}(\boldsymbol{y}) \in \mathbf{C}^{m_2 \times m_2}$, $\boldsymbol{H}(\boldsymbol{z}) \in \mathbf{C}^{m \times m}$ 分别表示复状态向量 $\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}$ 的函数; $\boldsymbol{f}(\boldsymbol{x}) \in \mathbf{C}^{m_1}$, $\boldsymbol{g}(\boldsymbol{y}) \in \mathbf{C}^{m_2}$, $\boldsymbol{h}(\boldsymbol{z}) \in \mathbf{C}^m$ 为非线性复函数向量; $\boldsymbol{u}(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) \in \mathbf{C}^m$ 为控制复向量。

定义 对驱动系统式(1), 驱动系统式(2)及响应系统式(3), 如果存在复矢量映射 $\phi: \mathbf{C}^{m_1} \rightarrow \mathbf{C}^m$, $\psi: \mathbf{C}^{m_2} \rightarrow \mathbf{C}^m$ 及复控制器 $\boldsymbol{u}(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z})$, 使得

$$\lim_{t \rightarrow \infty} \|\boldsymbol{z} - \phi(\boldsymbol{x}) - \psi(\boldsymbol{y})\| = 0 \quad (4)$$

$$\left. \begin{aligned} \boldsymbol{u}(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) &= -\boldsymbol{h}(\boldsymbol{z}) + \boldsymbol{J}(\phi)\boldsymbol{f}(\boldsymbol{x}) + \boldsymbol{J}(\psi)\boldsymbol{g}(\boldsymbol{y}) + \boldsymbol{J}(\phi)\boldsymbol{F}(\boldsymbol{x})\widehat{\boldsymbol{A}} + \boldsymbol{J}(\psi)\boldsymbol{G}(\boldsymbol{y})\widehat{\boldsymbol{B}} - \boldsymbol{H}(\boldsymbol{z})\widehat{\boldsymbol{C}} - \boldsymbol{K}\boldsymbol{e} \\ \boldsymbol{u}_r(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) &= -\boldsymbol{h}_r(\boldsymbol{z}) + \boldsymbol{J}_r(\phi)\boldsymbol{f}_r(\boldsymbol{x}) - \boldsymbol{J}_i(\phi)\boldsymbol{f}_i(\boldsymbol{x}) + \boldsymbol{J}_r(\psi)\boldsymbol{g}_r(\boldsymbol{y}) - \boldsymbol{J}_i(\psi)\boldsymbol{g}_i(\boldsymbol{y}) \\ &\quad + [\boldsymbol{J}_r(\phi)\boldsymbol{F}_r(\boldsymbol{x}) - \boldsymbol{J}_i(\phi)\boldsymbol{F}_i(\boldsymbol{x})]\widehat{\boldsymbol{A}} + [\boldsymbol{J}_r(\psi)\boldsymbol{G}_r(\boldsymbol{y}) - \boldsymbol{J}_i(\psi)\boldsymbol{G}_i(\boldsymbol{y})]\widehat{\boldsymbol{B}} - \boldsymbol{H}_r(\boldsymbol{z})\widehat{\boldsymbol{C}} - \boldsymbol{K}\boldsymbol{e}_r \\ \boldsymbol{u}_i(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) &= -\boldsymbol{h}_i(\boldsymbol{z}) + \boldsymbol{J}_r(\phi)\boldsymbol{f}_i(\boldsymbol{x}) + \boldsymbol{J}_i(\phi)\boldsymbol{f}_r(\boldsymbol{x}) + \boldsymbol{J}_r(\psi)\boldsymbol{g}_i(\boldsymbol{y}) + \boldsymbol{J}_i(\psi)\boldsymbol{g}_r(\boldsymbol{y}) \\ &\quad + [\boldsymbol{J}_r(\phi)\boldsymbol{F}_i(\boldsymbol{x}) + \boldsymbol{J}_i(\phi)\boldsymbol{F}_r(\boldsymbol{x})]\widehat{\boldsymbol{A}} + [\boldsymbol{J}_r(\psi)\boldsymbol{G}_i(\boldsymbol{y}) + \boldsymbol{J}_i(\psi)\boldsymbol{G}_r(\boldsymbol{y})]\widehat{\boldsymbol{B}} - \boldsymbol{H}_i(\boldsymbol{z})\widehat{\boldsymbol{C}} - \boldsymbol{K}\boldsymbol{e}_i \end{aligned} \right\} \quad (6)$$

$$\left. \begin{aligned} \dot{\widehat{\boldsymbol{A}}} = \dot{\widehat{\boldsymbol{A}}} &= -[\boldsymbol{J}_r(\phi)\boldsymbol{F}_r(\boldsymbol{x}) - \boldsymbol{J}_i(\phi)\boldsymbol{F}_i(\boldsymbol{x})]^\top \boldsymbol{e}_r - [\boldsymbol{J}_r(\phi)\boldsymbol{F}_i(\boldsymbol{x}) + \boldsymbol{J}_i(\phi)\boldsymbol{F}_r(\boldsymbol{x})]^\top \boldsymbol{e}_i - \boldsymbol{K}_A \widetilde{\boldsymbol{A}} \\ \dot{\widehat{\boldsymbol{B}}} = \dot{\widehat{\boldsymbol{B}}} &= -[\boldsymbol{J}_r(\psi)\boldsymbol{G}_r(\boldsymbol{y}) - \boldsymbol{J}_i(\psi)\boldsymbol{G}_i(\boldsymbol{y})]^\top \boldsymbol{e}_r - [\boldsymbol{J}_r(\psi)\boldsymbol{G}_i(\boldsymbol{y}) + \boldsymbol{J}_i(\psi)\boldsymbol{G}_r(\boldsymbol{y})]^\top \boldsymbol{e}_i - \boldsymbol{K}_B \widetilde{\boldsymbol{B}} \\ \dot{\widehat{\boldsymbol{C}}} = \dot{\widehat{\boldsymbol{C}}} &= [\boldsymbol{H}_r(\boldsymbol{z})]^\top \boldsymbol{e}_r + [\boldsymbol{H}_i(\boldsymbol{z})]^\top \boldsymbol{e}_i - \boldsymbol{K}_C \widetilde{\boldsymbol{C}} \end{aligned} \right\} \quad (7)$$

成立, 则称系统式(1), 系统式(2)和系统式(3)实现了广义组合复同步。

值得一提的是, 广义组合复同步是许多同步类型的推广, 如当 $\phi(\boldsymbol{x}) = 0$ 或 $\psi(\boldsymbol{y}) = 0$ 时, 为广义复同步; 当 $\phi(\boldsymbol{x}) = 0$, $\psi(\boldsymbol{y}) = 0$ 时, 为系统式(3)的混沌控制; 当 $\phi(\boldsymbol{x}) = \boldsymbol{\Lambda}_1(t)\boldsymbol{x}$, $\psi(\boldsymbol{y}) = \boldsymbol{\Lambda}_2(t)\boldsymbol{y}$, $\boldsymbol{\Lambda}_1(t) \in \mathbf{C}^{m_1 \times m_1}$, $\boldsymbol{\Lambda}_2(t) \in \mathbf{C}^{m_2 \times m_2}$ 时, 为函数投影组合复同步, 若 $\boldsymbol{\Lambda}_1(t) = 0$ 或 $\boldsymbol{\Lambda}_2(t) = 0$, 为函数投影复同步; 当 $\phi(\boldsymbol{x}) = \boldsymbol{\alpha}_1\boldsymbol{x}$, $\psi(\boldsymbol{y}) = \boldsymbol{\alpha}_2\boldsymbol{y}$, $\boldsymbol{\alpha}_1 \in \mathbf{C}^{m_1 \times m_1}$, $\boldsymbol{\alpha}_2 \in \mathbf{C}^{m_2 \times m_2}$ 时, 为组合复同步等。

定义广义组合复同步误差为 $\boldsymbol{e} = \boldsymbol{z} - \phi(\boldsymbol{x}) - \psi(\boldsymbol{y})$, 对其关于时间求导, 并将式(1), 式(2)和式(3)代入其中, 可得同步误差动力系统为

$$\left. \begin{aligned} \dot{\boldsymbol{e}} &= \dot{\boldsymbol{z}} - \boldsymbol{J}(\phi)\dot{\boldsymbol{x}} - \boldsymbol{J}(\psi)\dot{\boldsymbol{y}} \\ &= \boldsymbol{h}(\boldsymbol{z}) - \boldsymbol{J}(\phi)\boldsymbol{f}(\boldsymbol{x}) - \boldsymbol{J}(\psi)\boldsymbol{g}(\boldsymbol{y}) - \boldsymbol{J}(\phi)\boldsymbol{F}(\boldsymbol{x})\boldsymbol{A} \\ &\quad - \boldsymbol{J}(\psi)\boldsymbol{G}(\boldsymbol{y})\boldsymbol{B} + \boldsymbol{H}(\boldsymbol{z})\boldsymbol{C} + \boldsymbol{u}(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) \\ \dot{\boldsymbol{e}}_r &= \boldsymbol{h}_r(\boldsymbol{z}) - \boldsymbol{J}_r(\phi)\boldsymbol{f}_r(\boldsymbol{x}) + \boldsymbol{J}_i(\phi)\boldsymbol{f}_i(\boldsymbol{x}) \\ &\quad - \boldsymbol{J}_r(\psi)\boldsymbol{g}_r(\boldsymbol{y}) + \boldsymbol{J}_i(\psi)\boldsymbol{g}_i(\boldsymbol{y}) \\ &\quad - [\boldsymbol{J}_r(\phi)\boldsymbol{F}_r(\boldsymbol{x}) - \boldsymbol{J}_i(\phi)\boldsymbol{F}_i(\boldsymbol{x})]\boldsymbol{A} \\ &\quad - [\boldsymbol{J}_r(\psi)\boldsymbol{G}_r(\boldsymbol{y}) - \boldsymbol{J}_i(\psi)\boldsymbol{G}_i(\boldsymbol{y})]\boldsymbol{B} \\ &\quad + \boldsymbol{H}_r(\boldsymbol{z})\boldsymbol{C} + \boldsymbol{u}_r(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) \\ \dot{\boldsymbol{e}}_i &= \boldsymbol{h}_i(\boldsymbol{z}) - \boldsymbol{J}_r(\phi)\boldsymbol{f}_i(\boldsymbol{x}) - \boldsymbol{J}_i(\phi)\boldsymbol{f}_r(\boldsymbol{x}) \\ &\quad - \boldsymbol{J}_r(\psi)\boldsymbol{g}_i(\boldsymbol{y}) - \boldsymbol{J}_i(\psi)\boldsymbol{g}_r(\boldsymbol{y}) \\ &\quad - [\boldsymbol{J}_r(\phi)\boldsymbol{F}_i(\boldsymbol{x}) + \boldsymbol{J}_i(\phi)\boldsymbol{F}_r(\boldsymbol{x})]\boldsymbol{A} \\ &\quad - [\boldsymbol{J}_r(\psi)\boldsymbol{G}_i(\boldsymbol{y}) + \boldsymbol{J}_i(\psi)\boldsymbol{G}_r(\boldsymbol{y})]\boldsymbol{B} \\ &\quad + \boldsymbol{H}_i(\boldsymbol{z})\boldsymbol{C} + \boldsymbol{u}_i(\boldsymbol{x}, \boldsymbol{y}, \boldsymbol{z}) \end{aligned} \right\} \quad (5)$$

其中, $\boldsymbol{J}(\phi)$, $\boldsymbol{J}(\psi)$ 分别表示 $\phi(\boldsymbol{x})$, $\psi(\boldsymbol{y})$ 的雅可比矩阵。据此, 系统式(1), 系统式(2), 系统式(3)的广义组合同步问题转化为误差动力系统式(5)的零解稳定性问题。

3 自适应广义组合复同步设计

定理 如果复控制器及未知参数更新律为

则响应系统式(3)和驱动系统式(1), 驱动系统式(2)间实现了广义组合复同步, 同时未知参数得以成功辨识。其中 $\tilde{\mathbf{A}}, \tilde{\mathbf{B}}, \tilde{\mathbf{C}}$ 为未知参数向量 $\mathbf{A}, \mathbf{B}, \mathbf{C}$ 的估计值向量; $\tilde{\mathbf{A}} = \tilde{\mathbf{A}} - \mathbf{A}, \tilde{\mathbf{B}} = \tilde{\mathbf{B}} - \mathbf{B}, \tilde{\mathbf{C}} = \tilde{\mathbf{C}} - \mathbf{C}$ 为参数估计误差向量; $\mathbf{K} = \text{diag}(k_1, k_2, \dots, k_m)$, $\mathbf{K}_A = \text{diag}(k_{A,1}, k_{A,2}, \dots, k_{A,m_1})$, $\mathbf{K}_B = \text{diag}(k_{B,1}, k_{B,2}, \dots, k_{B,m_2})$, $\mathbf{K}_C = \text{diag}(k_{C,1}, k_{C,2}, \dots, k_{C,n})$ 为同步误差及参数误差反馈增益矩阵, 其元素均取正值。

证明 选取式(8)所示的 Lyapunov 函数:

$$\mathbf{V} = \frac{1}{2} \left[(\mathbf{e}_r)^T \mathbf{e}_r + (\mathbf{e}_i)^T \mathbf{e}_i + \tilde{\mathbf{A}}^T \tilde{\mathbf{A}} + \tilde{\mathbf{B}}^T \tilde{\mathbf{B}} + \tilde{\mathbf{C}}^T \tilde{\mathbf{C}} \right] \quad (8)$$

对式(8)关于时间求导, 并将式(5)代入其中, 可得

$$\begin{aligned} \dot{\mathbf{V}} &= (\dot{\mathbf{e}}_r)^T \mathbf{e}_r + (\dot{\mathbf{e}}_i)^T \mathbf{e}_i + \tilde{\mathbf{A}}^T \dot{\tilde{\mathbf{A}}} + \tilde{\mathbf{B}}^T \dot{\tilde{\mathbf{B}}} + \tilde{\mathbf{C}}^T \dot{\tilde{\mathbf{C}}} \\ &= \left\{ \mathbf{h}_r(\mathbf{z}) - \mathbf{J}_r(\phi) \mathbf{f}_r(\mathbf{x}) + \mathbf{J}_i(\phi) \mathbf{f}_i(\mathbf{x}) \right. \\ &\quad - \mathbf{J}_r(\psi) \mathbf{g}_r(\mathbf{y}) + \mathbf{J}_i(\psi) \mathbf{g}_i(\mathbf{y}) \\ &\quad - [\mathbf{J}_r(\phi) \mathbf{F}_r(\mathbf{x}) - \mathbf{J}_i(\phi) \mathbf{F}_i(\mathbf{x})] \mathbf{A} \\ &\quad - [\mathbf{J}_r(\psi) \mathbf{G}_r(\mathbf{y}) - \mathbf{J}_i(\psi) \mathbf{G}_i(\mathbf{y})] \mathbf{B} \\ &\quad \left. + \mathbf{H}_r(\mathbf{z}) \mathbf{C} + \mathbf{u}_r(\mathbf{x}, \mathbf{y}, \mathbf{z}) \right\}^T \mathbf{e}_r \\ &\quad + \left\{ \mathbf{h}_i(\mathbf{z}) - \mathbf{J}_r(\phi) \mathbf{f}_i(\mathbf{x}) - \mathbf{J}_i(\phi) \mathbf{f}_r(\mathbf{x}) \right. \\ &\quad - \mathbf{J}_r(\psi) \mathbf{g}_i(\mathbf{y}) - \mathbf{J}_i(\psi) \mathbf{g}_r(\mathbf{y}) \\ &\quad - [\mathbf{J}_r(\phi) \mathbf{F}_i(\mathbf{x}) + \mathbf{J}_i(\phi) \mathbf{F}_r(\mathbf{x})] \mathbf{A} \\ &\quad - [\mathbf{J}_r(\psi) \mathbf{G}_i(\mathbf{y}) + \mathbf{J}_i(\psi) \mathbf{G}_r(\mathbf{y})] \mathbf{B} \\ &\quad \left. + \mathbf{H}_i(\mathbf{z}) \mathbf{C} + \mathbf{u}_i(\mathbf{x}, \mathbf{y}, \mathbf{z}) \right\}^T \mathbf{e}_i \\ &\quad + \tilde{\mathbf{A}}^T \dot{\tilde{\mathbf{A}}} + \tilde{\mathbf{B}}^T \dot{\tilde{\mathbf{B}}} + \tilde{\mathbf{C}}^T \dot{\tilde{\mathbf{C}}} \end{aligned} \quad (9)$$

将式(6)和式(7)代入式(9), 可得

$$\begin{aligned} \dot{\mathbf{V}} &= \left\{ [\mathbf{J}_r(\phi) \mathbf{F}_r(\mathbf{x}) - \mathbf{J}_i(\phi) \mathbf{F}_i(\mathbf{x})] \tilde{\mathbf{A}} + [\mathbf{J}_r(\psi) \mathbf{G}_r(\mathbf{y}) \right. \\ &\quad - \mathbf{J}_i(\psi) \mathbf{G}_i(\mathbf{y})] \tilde{\mathbf{B}} - \mathbf{H}_r(\mathbf{z}) \tilde{\mathbf{C}} - \mathbf{K} \mathbf{e}_r \left. \right\}^T \mathbf{e}_r \\ &\quad + \left\{ [\mathbf{J}_r(\phi) \mathbf{F}_i(\mathbf{x}) + \mathbf{J}_i(\phi) \mathbf{F}_r(\mathbf{x})] \tilde{\mathbf{A}} \right. \\ &\quad + [\mathbf{J}_r(\psi) \mathbf{G}_i(\mathbf{y}) + \mathbf{J}_i(\psi) \mathbf{G}_r(\mathbf{y})] \tilde{\mathbf{B}} \\ &\quad \left. - \mathbf{H}_i(\mathbf{z}) \tilde{\mathbf{C}} - \mathbf{K} \mathbf{e}_i \right\}^T \mathbf{e}_i \\ &\quad + \tilde{\mathbf{A}}^T \left\{ -[\mathbf{J}_r(\phi) \mathbf{F}_r(\mathbf{x}) - \mathbf{J}_i(\phi) \mathbf{F}_i(\mathbf{x})]^T \mathbf{e}_r \right. \\ &\quad - [\mathbf{J}_r(\phi) \mathbf{F}_i(\mathbf{x}) + \mathbf{J}_i(\phi) \mathbf{F}_r(\mathbf{x})]^T \mathbf{e}_i - \mathbf{K}_A \tilde{\mathbf{A}} \left. \right\} \\ &\quad + \tilde{\mathbf{B}}^T \left\{ -[\mathbf{J}_r(\psi) \mathbf{G}_r(\mathbf{y}) - \mathbf{J}_i(\psi) \mathbf{G}_i(\mathbf{y})]^T \mathbf{e}_r \right. \\ &\quad - [\mathbf{J}_r(\psi) \mathbf{G}_i(\mathbf{y}) + \mathbf{J}_i(\psi) \mathbf{G}_r(\mathbf{y})]^T \mathbf{e}_i - \mathbf{K}_B \tilde{\mathbf{B}} \left. \right\} \\ &\quad + \tilde{\mathbf{C}}^T \left\{ [\mathbf{H}_r(\mathbf{z})]^T \mathbf{e}_r + [\mathbf{H}_i(\mathbf{z})]^T \mathbf{e}_i - \mathbf{K}_C \tilde{\mathbf{C}} \right\} \\ &= -(\mathbf{e}_r)^T \mathbf{K} \mathbf{e}_r - (\mathbf{e}_i)^T \mathbf{K} \mathbf{e}_i - \tilde{\mathbf{A}}^T \mathbf{K}_A \tilde{\mathbf{A}} \\ &\quad - \tilde{\mathbf{B}}^T \mathbf{K}_B \tilde{\mathbf{B}} - \tilde{\mathbf{C}}^T \mathbf{K}_C \tilde{\mathbf{C}} < 0 \end{aligned} \quad (10)$$

根据 Lyapunov 稳定性理论, 当 $\mathbf{V} > 0$ 且 $\dot{\mathbf{V}} < 0$ 时, 随着时间的推移, 同步误差及参数误差渐近趋向于 0, 则同步误差动力系统式(5)和参数估计误差系统式(7)具有稳定的零解, 即实现了响应系统式(3)和驱动系统式(1), 驱动系统式(2)间的广义组合复同步及未知参数的辨识。

4 数值仿真与分析

为了验证上述广义组合复同步及参数辨识方法的正确性, 在此选择式(11), 式(12)和式(13)所示的超混沌复 Lorenz 系统、超混沌复 Chen 系统、超混沌复 Lü 系统分别作为驱动系统和响应系统^[2]。由于已有文献对此 3 个超混沌复系统的动力学行为进行分析, 在此不再赘述。

$$\left. \begin{aligned} \dot{x}_1 &= a_1(x_2 - x_1) + x_4 \\ \dot{x}_2 &= a_2 x_1 - x_2 - x_1 x_3 \\ \dot{x}_3 &= (\bar{x}_1 x_2 + x_1 \bar{x}_2) / 2 - a_3 x_3 + x_4 \\ \dot{x}_4 &= (\bar{x}_1 x_2 + x_1 \bar{x}_2) / 2 - a_4 x_4 \end{aligned} \right\} \quad (11)$$

$$\left. \begin{aligned} \dot{y}_1 &= b_1(y_2 - y_1) \\ \dot{y}_2 &= (b_2 - b_1)y_1 - y_1 y_3 + b_2 y_2 + y_4 \\ \dot{y}_3 &= (\bar{y}_1 y_2 + y_1 \bar{y}_2) / 2 - b_3 y_3 + y_4 \\ \dot{y}_4 &= (\bar{y}_1 y_2 + y_1 \bar{y}_2) / 2 - b_4 y_4 \end{aligned} \right\} \quad (12)$$

$$\left. \begin{aligned} \dot{z}_1 &= c_1(z_2 - z_1) + z_4 + u_1 \\ \dot{z}_2 &= c_2 z_2 - z_1 z_3 + z_4 + u_2 \\ \dot{z}_3 &= (\bar{z}_1 z_2 + z_1 \bar{z}_2) / 2 - c_3 z_3 + u_3 \\ \dot{z}_4 &= (\bar{z}_1 z_2 + z_1 \bar{z}_2) / 2 - c_4 z_4 + u_4 \end{aligned} \right\} \quad (13)$$

为了应用文中第 3 节所提控制器、参数辨识的设计方法, 可将系统式(11), 系统式(12)和系统式(13)表示成式(1), 式(2)和式(3)的形式, 其中 $\mathbf{A} = [a_1 \ a_2 \ a_3 \ a_4]^T$, $\mathbf{B} = [b_1 \ b_2 \ b_3 \ b_4]^T$, $\mathbf{C} = [c_1 \ c_2 \ c_3 \ c_4]^T$, $\mathbf{u} = [u_1 \ u_2 \ u_3 \ u_4]^T$,

$$\mathbf{F}(\mathbf{x}) = \begin{bmatrix} x_2 - x_1 & 0 & 0 & 0 \\ 0 & x_1 & 0 & 0 \\ 0 & 0 & -x_3 & 0 \\ 0 & 0 & 0 & -x_4 \end{bmatrix}$$

$$\mathbf{f}(\mathbf{x}) = \begin{bmatrix} x_4 \\ -x_2 - x_1 x_3 \\ (\bar{x}_1 x_2 + x_1 \bar{x}_2) / 2 + x_4 \\ (\bar{x}_1 x_2 + x_1 \bar{x}_2) / 2 \end{bmatrix}$$

$$\begin{aligned}
 \mathbf{G}(\mathbf{y}) &= \begin{bmatrix} y_2 - y_1 & 0 & 0 & 0 \\ -y_1 & y_1 & 0 & 0 \\ 0 & 0 & -y_3 & 0 \\ 0 & 0 & 0 & -y_4 \end{bmatrix} \\
 \mathbf{g}(\mathbf{y}) &= \begin{bmatrix} 0 \\ -y_1 y_3 + b_2 y_2 + y_4 \\ (\bar{y}_1 y_2 + y_1 \bar{y}_2)/2 + y_4 \\ (\bar{y}_1 y_2 + y_1 \bar{y}_2)/2 \end{bmatrix} \\
 \mathbf{H}(\mathbf{z}) &= \begin{bmatrix} z_2 - z_1 & 0 & 0 & 0 \\ 0 & z_2 & 0 & 0 \\ 0 & 0 & -z_3 & 0 \\ 0 & 0 & 0 & -z_4 \end{bmatrix} \\
 \mathbf{h}(\mathbf{z}) &= \begin{bmatrix} z_4 \\ -z_1 z_3 + z_4 \\ (\bar{z}_1 z_2 + z_1 \bar{z}_2)/2 \\ (\bar{z}_1 z_2 + z_1 \bar{z}_2)/2 \end{bmatrix}
 \end{aligned}$$

为不失一般性，选取式(14)所示的复映射向量

$$\left. \begin{aligned}
 \phi(\mathbf{x}) &= [jx_2 \ jx_1 \ x_4 \ x_3]^T \\
 \psi(\mathbf{y}) &= [(1+j)y_1 - jy_2 \ y_3 \ y_3 y_4 / 10]^T
 \end{aligned} \right\} \quad (14)$$

其对应的雅可比矩阵为

$$\left. \begin{aligned}
 \mathbf{J}(\phi) &= \begin{bmatrix} 0 & j & 0 & 0 \\ j & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \end{bmatrix} \\
 \mathbf{J}(\psi) &= \begin{bmatrix} 1+j & 0 & 0 & 0 \\ 0 & -j & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & y_4/10 & y_3/10 \end{bmatrix}
 \end{aligned} \right\} \quad (15)$$

则根据式(6)和式(7)，可设计同步控制器如式(16)，3个系统未知参数更新律如式(17)，式(18)和式(19)。

$$\left. \begin{aligned}
 u_{1,r} &= -z_4 + x_{2,i} + x_{1,i} x_3 - x_{1,i} \hat{a}_2 + (y_{2,r} - y_{1,r} - y_{2,i} + y_{1,i}) \hat{b}_1 - (z_{2,r} - z_{1,r}) \hat{c}_1 - k_1 e_{1,r} \\
 u_{1,i} &= -x_{2,r} - x_{1,r} x_3 + x_{1,r} \hat{a}_2 + (y_{2,r} - y_{1,r} + y_{2,i} - y_{1,i}) \hat{b}_1 - (z_{2,i} - z_{1,i}) \hat{c}_1 - k_1 e_{1,i} \\
 u_{2,r} &= z_{1,r} z_3 - z_4 - y_{1,i} y_3 - (x_{2,i} - x_{1,i}) \hat{a}_1 - y_{1,i} \hat{b}_1 + (y_{2,i} + y_{1,i}) \hat{b}_2 - z_{2,r} \hat{c}_2 - k_2 e_{2,r} \\
 u_{2,i} &= z_{1,i} z_3 + x_4 + y_{1,r} y_3 - y_4 + (x_{2,r} - x_{1,r}) \hat{a}_1 + y_{1,r} \hat{b}_1 - (y_{2,r} + y_{1,r}) \hat{b}_2 - z_{2,i} \hat{c}_2 - k_2 e_{2,i} \\
 u_3 &= -z_{1,r} z_{2,r} - z_{1,i} z_{2,i} + x_{1,r} x_{2,r} + x_{1,i} x_{2,i} + y_{1,r} y_{2,r} + y_{1,i} y_{2,i} + y_4 - x_4 \hat{a}_4 - y_3 \hat{b}_3 + z_3 \hat{c}_3 - k_3 e_3 \\
 u_4 &= -z_{1,r} z_{2,r} - z_{1,i} z_{2,i} + x_{1,r} x_{2,r} + x_{1,i} x_{2,i} + x_4 + (y_3 + y_4)(y_{1,r} y_{2,r} + y_{1,i} y_{2,i}) / 10 + y_4^2 / 10 \\
 &\quad - x_3 \hat{a}_3 - y_3 y_4 (\hat{b}_3 + \hat{b}_4) / 10 + z_4 \hat{c}_4 - k_4 e_4
 \end{aligned} \right\} \quad (16)$$

$$\left. \begin{aligned}
 \dot{\hat{a}}_1 &= (x_{2,i} - x_{1,i}) e_{2,r} - (x_{2,r} - x_{1,r}) e_{2,i} - k_{A,1} (\hat{a}_1 - a_1) \\
 \dot{\hat{a}}_2 &= x_{1,i} e_{1,r} - x_{1,r} e_{1,i} - k_{A,2} (\hat{a}_2 - a_2) \\
 \dot{\hat{a}}_3 &= x_3 e_4 - k_{A,3} (\hat{a}_3 - a_3) \\
 \dot{\hat{a}}_4 &= x_4 e_3 - k_{A,4} (\hat{a}_4 - a_4)
 \end{aligned} \right\} \quad (17)$$

其中，

$$\begin{aligned}
 e_{1,r} &= z_{1,r} + x_{2,i} - y_{1,r} + y_{1,i} \\
 e_{1,i} &= z_{1,i} - x_{2,r} - y_{1,r} - y_{1,i} \\
 e_{2,r} &= z_{2,r} + x_{1,i} - y_{2,i} \\
 e_{2,i} &= z_{2,i} - x_{1,r} + y_{2,r} \\
 e_3 &= z_3 - x_4 - y_3 \\
 e_4 &= z_4 - x_3 - y_3 y_4 / 10
 \end{aligned}$$

$$\left. \begin{aligned}
 \dot{\hat{b}}_1 &= (y_{2,r} - y_{1,r} - y_{2,i} + y_{1,i}) e_{1,r} - (y_{2,r} - y_{1,r} + y_{2,i} - y_{1,i}) \\
 &\quad \cdot e_{1,i} + y_{1,i} e_{2,r} - y_{1,r} e_{2,i} - k_{B,1} (\hat{b}_1 - b_1) \\
 \dot{\hat{b}}_2 &= -(y_{2,i} + y_{1,i}) e_{2,r} + (y_{2,r} + y_{1,r}) e_{2,i} - k_{B,2} (\hat{b}_2 - b_2) \\
 \dot{\hat{b}}_3 &= y_3 e_3 + y_3 y_4 e_4 / 10 - k_{B,3} (\hat{b}_3 - b_3) \\
 \dot{\hat{b}}_4 &= y_3 y_4 e_4 / 10 - k_{B,4} (\hat{b}_4 - b_4)
 \end{aligned} \right\} \quad (18)$$

$$\left. \begin{aligned}
 \dot{\hat{c}}_1 &= (z_{2,r} - z_{1,r}) e_{1,r} + (z_{2,i} - z_{1,i}) e_{1,i} - k_{C,1} (\hat{c}_1 - c_1) \\
 \dot{\hat{c}}_2 &= z_{2,r} e_{2,r} + z_{2,i} e_{2,i} - k_{C,2} (\hat{c}_2 - c_2) \\
 \dot{\hat{c}}_3 &= -z_3 e_3 - k_{C,3} (\hat{c}_3 - c_3) \\
 \dot{\hat{c}}_4 &= -z_4 e_4 - k_{C,4} (\hat{c}_4 - c_4)
 \end{aligned} \right\} \quad (19)$$

为了得到同步及参数辨识结果，我们基于 Matlab 进行数值模拟，并按文献[12]将未知参数的真实值设定为 $\mathbf{A} = [a_1 \ a_2 \ a_3 \ a_4]^T = [8 \ 50 \ 5 \ 15]^T$ ， $\mathbf{B} = [b_1 \ b_2 \ b_3 \ b_4]^T = [36 \ 25 \ 4 \ 5]^T$ ， $\mathbf{C} = [c_1 \ c_2 \ c_3 \ c_4]^T = [42 \ 25 \ 6 \ 5]^T$ ，以确保系统处于超混沌状态；3个系统初始状态分别设置为 $\mathbf{x}(0) = [2 - j \ 5.8 - 2j \ -12 \ -16]^T$ ， $\mathbf{y}(0) = [1.7 + 2.3j \ 0.1 - 14j \ -16 \ -18]^T$ ， $\mathbf{z}(0) = [3.6 - 0.6j \ 0.9 - j \ 13 \ 15]^T$ ；未知参数估计值的初值均设为 0；同步误差及参数误差反馈增益 $k_l = k_{A,l} = k_{B,l} = k_{C,l} = 10$ ($l = 1, 2, 3, 4$)，则仿真结果如图 1-图 3 所示。图 1 给出了响应系统状态广义组合复同步于驱动系统状态的过程，图 2 刻画了广义

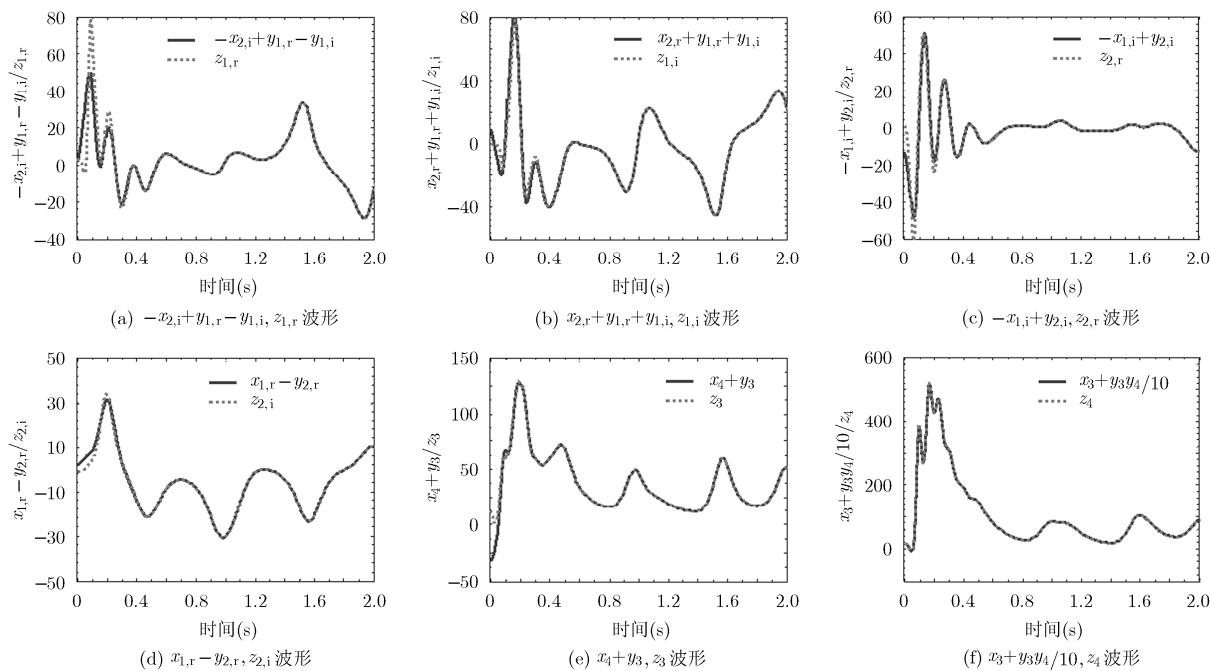


图 1 广义组合复同步过程 ($k_l = k_{A,l} = k_{B,l} = k_{C,l} = 10$ ($l = 1, 2, 3, 4$))

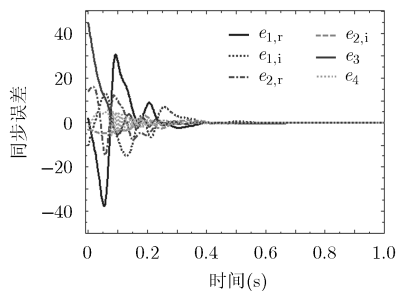


图 2 广义组合复同步误差 ($k_l = k_{A,l} = k_{B,l} = k_{C,l} = 10$ ($l = 1, 2, 3, 4$))

组合复同步误差渐近趋于 0 的过程，图 1 和图 2 一致表明广义组合复同步能在极短的时间内成功实现；而图 3(a)，图 3 (b)和图 3 (c)分别给出了对系统式(11)，系统式(12)和系统式(13)未知参数的辨识过程，结果表明未知参数的估计值渐近趋于其真实值，成功实现了未知参数的准确辨识。

为了分析误差反馈增益对同步收敛速度的影响，将各反馈增益修改为 $k_l = k_{A,l} = k_{B,l} = k_{C,l} = 1$ ($l = 1, 2, 3, 4$)，而保持其他参数和初始条件不变，再次进行仿真，得到图 4 所示的广义组合复同步误差图。通过对图 2 和图 4 的比较，容易得出：反馈增益减小，即控制强度减弱时，自适应广义组合复同步速度减慢，系统需要经历更长的时间才能达成同步。因此，通过调节误差反馈增益，可以有效控制同步速度。

5 结束语

本文针对一类含有未知参数的异结构超混沌复系统，提出了一种自适应广义组合复同步及参数辨识方法。首先，基于自适应控制和 Lyapunov 稳定性理论，从理论上设计了非线性反馈控制器及参数估计更新律，并给予了证明。然后，将所提方法应用于超混沌复 Lorenz 系统、超混沌复 Chen 系统、超

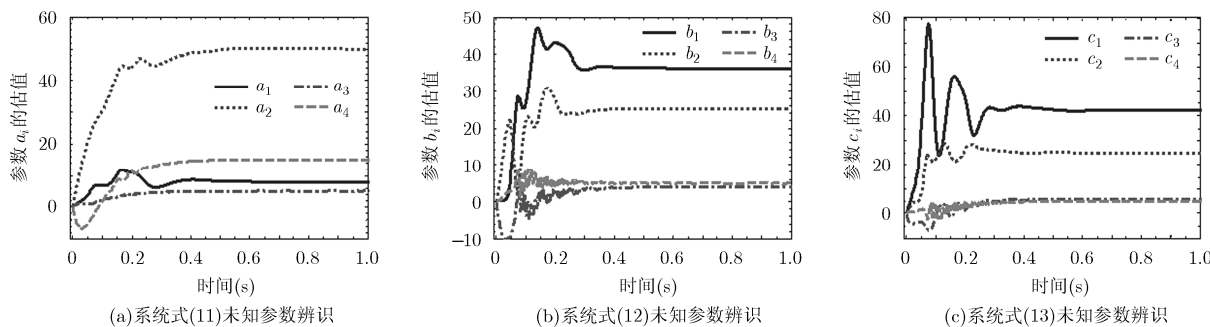


图 3 未知参数辨识过程 ($k_l = k_{A,l} = k_{B,l} = k_{C,l} = 10$ ($l = 1, 2, 3, 4$))

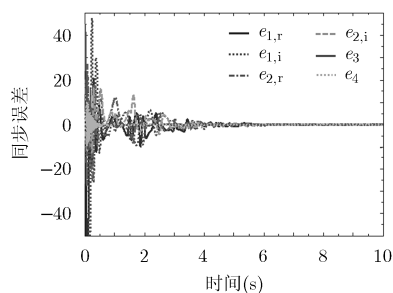


图 4 广义组合复同步误差 ($k_l = k_{A,l} = k_{B,l} = k_{C,l} = 1$ ($l = 1, 2, 3, 4$))

混沌复 Lü 系统的广义组合复同步及参数估计, 从数值仿真角度验证了该方法的正确性和有效性, 并表明误差反馈增益能有效调控同步的收敛速度。将来, 还会从电路仿真、电路实验的角度实现该方法, 以推动其在信号加密、混沌保密通信等领域的应用。

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